The effect of stress and magnetostriction on the anisotropy of CoNi/Pt multilayers

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Abstract

An attempt is made to correlate the effective magnetic anisotropy of sputtered CoNi/Pt multilayers to the average stress in the thin film. It was found that compressive film stress decreases the perpendicular magnetic anisotropy.

1. Introduction

Magneto-Optical (MO) multilayers are considered to be good candidates for future high-density MO recording [1,2]. From other research it is known (e.g. [3]) that there can be a considerable contribution of stress induced anisotropy to the total (perpendicular) anisotropy. To correlate this effective magnetic anisotropy to the average stress in the thin film, a series of sputtered Co₅₀Ni₅₀/Pt multilayers was prepared in which only the sputter pressure was varied. Each multilayer consists of a Pt seedlayer and a stack of 17 Co₅₀Ni₅₀/Pt bilayers. The experimental details about the deposition are given elsewhere [4].

2. Sample characterization

The properties of the deposited samples are listed in Table 1. The layer thicknesses tSeed, tCoNi and tPt were estimated from the product of sputter time and sputter rate. The bilayer thickness t_bilayer, measured by low angle XRD was found to be in good agreement with the projected layer thicknesses. The largest deviation was found for sample B (7%). Furthermore the saturation magnetization Mₛ was calculated using the CoNi thickness only and found to be 1060±60 kA/m for all films. Magnetic torque measurements were performed at room temperature at an applied field of 1330 kA/m. The effective anisotropies measured in this way, normalised to the magnetic volume, are also displayed in Table 1. To measure the film stress two different methods were applied: measurement of the surface curvature, and XRD measurements. The average internal film stress can be calculated from the measured radii of curvature and the lattice spacings respectively. The strain free lattice spacing, d₀ [Å], was determined in the following way: from the curvature measurements we know the pressure range at which the deposited multilayers are in a strain free situation, approximately 3.7×10⁻² [mbar]. The corresponding average lattice spacing as measured with the XRD was taken as d₀ and found to be 3.760±0.017 Å. Further experimental details about these methods can be found in Refs. [3,4]. Both methods deliver the results as depicted in Fig. 1a and b. Note that if the film stress is isotropic the equation given by Stoney [5] is used.

3. Anisotropy model

In order to correlate stress and magnetic anisotropy the following model was derived. For multilayers with interface anisotropy a semi-empirical formula [6] was used to determine the interface and bulk contributions:

\[ t_{\text{magn}} \cdot K_{\text{eff}} = 2K_S + K_V \cdot t_{\text{magn}}. \]  

The volume anisotropy \( K_V \) consists of crystal anisotropy \( K_A \) and demagnetization anisotropy \( K_D \). When a plane stress is homogeneously distributed throughout the magnetic layers of the multilayer, this will also add to the volume anisotropy by \( K_{\text{stress}} \), which is defined as \( K_{\text{stress}} = \)...

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1. Results and discussion

High angle XRD experiments revealed that the CoNi/Pt multilayers discussed here all had the fcc (111) structure. This corresponds to the fcc structure found in the phase diagram of bulk Co50Ni50. Due to the fcc structure, $K_1$ is small and negative: $K_1 = -108 \text{ kJ/m}^3$ for bulk Co50Ni50 [7]. Therefore for the following calculation it is assumed that the $K_1$ of the CoNi layers is $-108 \text{ kJ/m}^3$ over the whole argon pressure range. If we now perform the calculation according to Eq. (2), we arrive at $\lambda_5 = -130 \times 10^{-6}$ and $K_S = 0.285 \text{ mJ/m}^2$ for the curvature measurements and at $\lambda_5 = -56 \times 10^{-6}$ and $K_S = 0.287 \text{ mJ/m}^2$ for the stress measurements based on XRD.

We observe that the surface anisotropy values of both methods are very similar. The $K_S$ determined in this way compares well with results from magnetic layer thickness series from various authors (e.g. [8]). From this good match we conclude that the choice of the argon pressure at which the multilayer is in the stress-free state is justified.

Comparison of the saturation magnetostriction values reveals that the magnetostriction obtained by the surface curvature measurement is more than twice as large as that obtained from XRD results. A probable explanation is that during growth the thin film relaxes on a macroscopic scale, thereby reducing the curvature of the substrate. However, the stress measured with the XRD method gives a more realistic value of $\lambda_5$. With XRD the average lattice spacing is measured, which represents the stress state within the crystallites of the layer. As the stress anisotropy is also generated on this local scale, the XRD values are thought to be more representative in this case.

In conclusion we can say that both methods indicate that the magnetic anisotropy changes from perpendicular to in-plane with increasing compressive film stress. Therefore compressive film stress, which increases with decreasing argon pressure, is considered to be unfavourable for (perpendicular) magneto-optic recording.

Fig. 1. (a) Stress along the $R_1$, $R_2$ axes and the stress calculated according to Stoney’s equation. (b) Stress measured by XRD as a function of the argon pressure.

$$\frac{-3}{2} \lambda_5 \sigma,$$
with $\lambda_5$ the saturation magnetostriction and $\sigma$ the plane stress in the film. In this case a positive value for $\sigma$ denotes tensile stress. Together, the effective anisotropy is defined as:

$$K_{\text{eff}} = 2K_S / I_{\text{mags}} + K_1 - \frac{1}{2} \mu_0 M_s^2 - \frac{3}{2} \lambda_5 \sigma. \quad (2)$$

This equation is schematically shown in Fig. 2. Now the saturation magnetostriction and the surface anisotropy can be calculated as being $\lambda_5 = -\frac{3}{2} \tan \alpha$ and $K_S = \frac{1}{2} I_{\text{mags}} (P - K_1 + \frac{1}{2} \mu_0 M_s^2)$ respectively, where $P$ and $\alpha$ are defined in Fig. 2.

Fig. 2. Schematic representation of Eq. (1). The dashed lines indicate the $x$ and $y$ axis. The linear fit with slope $\alpha$ crosses the y-axis at point $P$.